

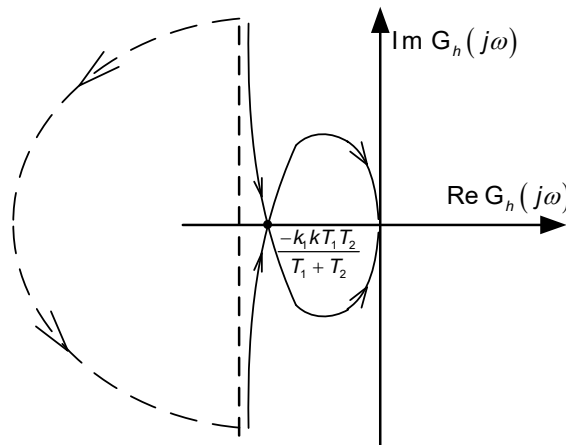
**SOLUTION OF EXAM 01**  
Subject: CONTROL THEORY

Exercise 1 (5 marks):

a) (1.5 marks)

i. (1.5 d)

i. (1d) We have:



(0.5d) Using Nyquist Property  $0 < k_1 < 2$

i. (0.5 d)

Because of stable closed loop system, there exists the Limitation

$$\lim_{t \rightarrow \infty} (u(t) - y(t)) = \lim_{s \rightarrow 0} s(U(s) - Y(s)) = \lim_{s \rightarrow 0} sU(s) \left( 1 - \frac{k_2 k_1 G(s)}{1 + k_1 G(s)} \right);$$

$$u(t) = 1(t) \text{ v\grave{a}} \lim_{s \rightarrow 0} G(s) = +\infty, \text{ we obtain } \lim_{t \rightarrow \infty} (u(t) - y(t)) = 1 - k_2$$

We imply  $k_2 = 1$ ;

b) (2 marks)

i. (1 mark)  $G(s) = \frac{k}{s(1 + T_2 s)^2}$

$$a = 4: T_I = T_1 + 4T_2, k_p = \frac{T_I}{8kT_2^2}, T_D = \frac{4T_1 T_2}{T_I}, T = 4T_2 \text{ with}$$

$$k = 0.5, T_1 = T_2 = 2 \text{ we obtain } T_I = 10, k_p = \frac{5}{8}, T_D = 1.6, T = 8$$

ii. (1 mark) Stability reserve of closed system does not depend on  $R_2(s)$ . We need to obtain the open system with transfer function:

$$\begin{aligned} G_h(s) &= R_1(s)G(s) = k_p \left( 1 + \frac{1}{T_I s} + T_D s \right) \cdot \frac{k}{s(1 + T_1 s)(1 + T_2 s)} \\ &= \frac{k_p(1 + T_A s)(1 + T_B s)}{T_I s} \cdot \frac{k}{s(1 + T_1 s)(1 + T_2 s)} = \frac{k_p k(1 + T_B s)}{T_I s^2(1 + T_2 s)} \end{aligned}$$

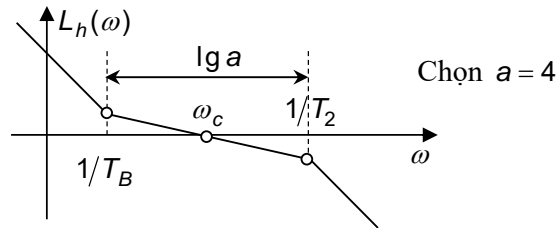
We select  $T_A = T_1$  with  $T_A + T_B = T_I$ ,  $T_A T_B = T_I T_D$ ,  $T_B = 4T_2 > T_2$ , we obtain the Bode diagram of open system as follows.

$$\omega_c = \frac{1}{\sqrt{T_B T_2}}$$

$T_B = 8, T_1 = T_2 = 2$  we imply  $\omega_c = \frac{1}{4}$ . Stability reserve of closed system  $\Delta\varphi$ :

$$\Delta\varphi = -\pi - \varphi_c = -\pi - \arctan(\omega_c T_2) - \arctan(\omega_c T_B)$$

$$\Delta\varphi = \arctan\left(\frac{1}{2}\right) - \arctan(2)$$



### Exercise 2

a) (1 marks) we denote

$$A = \begin{pmatrix} 1 & 0 & 1 \\ 0 & 2 & 1 \\ 0 & 1 & 1 \end{pmatrix}, B = \begin{pmatrix} 1 \\ 0 \\ 1 \end{pmatrix}, \underline{c} = \begin{pmatrix} a \\ 0 \\ 1 \end{pmatrix} \Rightarrow \begin{cases} \frac{d\underline{x}}{dt} = A\underline{x} + B\underline{u} \\ y = \underline{c}^T \underline{x} \end{cases}$$

i. (0.5 marks)

The equivalent polynomial of matrix  $A$  will be:

$$\det(sI - A) = (s-1)(s^2 - 3s + 1). \text{ This system is not stable;}$$

ii. (0.5 marks)  $\text{Rank}(B, AB, A^2B) = 3 \Rightarrow$  This system is controllable

b) (1 marks)

$$i. (0.5 \text{ marks}) N = \begin{pmatrix} \underline{c}^T \\ \underline{c}^T A \\ \underline{c}^T A^2 \end{pmatrix} = \begin{pmatrix} a & 0 & 1 \\ a & 1 & a+1 \\ a & a+3 & 2a+2 \end{pmatrix}$$

$$ii. (0.5 \text{ marks}) \det(N) = -a(a^2 + a - 1)$$

In order to obtain the observability property:  $\det(N) \neq 0 \Leftrightarrow a \neq 0; \frac{-1 \pm \sqrt{5}}{2}$

c) (2 marks)

i. (1 marks) State Feedback control is  $\underline{u} = \underline{w} - R\underline{x}$  với  $R = (r_1 \ r_2 \ r_3)$  satisfy eigen values of  $(A - \underline{b}r^T)$  inside  $(-2, 0)$  and we select all of eigen values

being -1), we obtain based on Ackermann

$$[r_1 \ r_2 \ r_3] = [0 \ 0 \ 1] M^{-1} \Phi_R(A) = [-4, -24, 11]$$

ii. (1 marks) Observer

i. (0.5 marks)  $\underline{\hat{x}}$  is the root of difference equation

$$\frac{d\underline{\hat{x}}}{dt} = A\underline{\hat{x}} + \underline{b}u + L(y - \underline{c}^T \underline{\hat{x}}).$$

ii. (0.5 marks) Find matrix  $L$  to obtain that  $(A - L\underline{c}^T)$  have all eigenvalues being -3 (faster than  $e^{-2t}$ ). Using Ackermann:

$$L = \Phi_L(A) N^{-1} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = [28, 77, -15]^T$$

(1d) **Drawing.** The closed system is not controllable because  $\underline{\hat{x}}$  converge to  $\underline{x}$

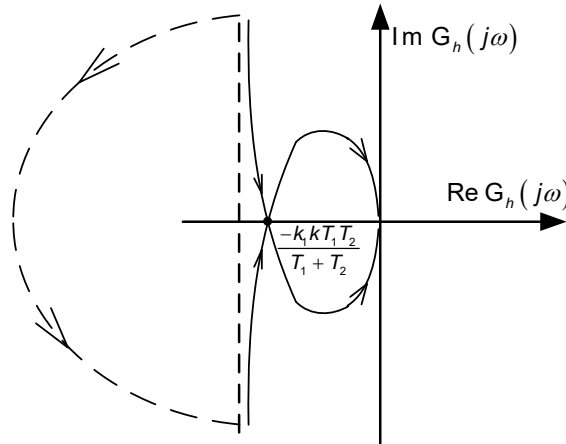
a) **(0.5 d)** Selecting the state feedback controller  $\underline{u} = \underline{\omega} - R\underline{x}$  with  $R = \begin{bmatrix} -4 & -24 & 11 \\ 0 & 0 & 0 \end{bmatrix}$

**SOLUTION OF EXAM 02**  
Subject: CONTROL THEORY

Exercise 1 (5 marks):

a) (1.5 marks)

i. (1.5 d) We have:



(0.5d)  $0 < k_1 < 0.2$

i. (0.5 d)

Because of stable closed loop system, there exists the Limitation

$$\lim_{t \rightarrow \infty} (u(t) - y(t)) = \lim_{s \rightarrow 0} s(U(s) - Y(s)) = \lim_{s \rightarrow 0} sU(s) \left( 1 - \frac{k_2 k_1 G(s)}{1 + k_1 G(s)} \right);$$

Because  $u(t) = 1(t)$ , we imply  $\lim_{s \rightarrow 0} G(s) = +\infty$  and

$$\lim_{t \rightarrow \infty} (u(t) - y(t)) = 1 - k_2, \text{ we obtain } k_2 = 1;$$

b) (2 marks)

i. (1 marks)  $G(s) = \frac{k}{s(1 + T_2 s)^2}$

(a = 4):  $T_I = T_1 + 4T_2$ ,  $k_p = \frac{T_I}{8kT_2^2}$ ,  $T_D = \frac{4T_1 T_2}{T_I}$ ,  $T = 4T_2$  where

$k = 10$ ,  $T_1 = T_2 = 1$  we obtain  $T_I = 5$ ,  $k_p = \frac{1}{16}$ ,  $T_D = 0.8$ ,  $T = 4$

ii. (1 mark) Stability reserve of closed system does not depend on  $R_2(s)$ . We need to obtain the open system with transfer function:

$$\begin{aligned} G_h(s) &= R_1(s)G(s) = k_p \left( 1 + \frac{1}{T_I s} + T_D s \right) \cdot \frac{k}{s(1 + T_1 s)(1 + T_2 s)} \\ &= \frac{k_p(1 + T_A s)(1 + T_B s)}{T_I s} \cdot \frac{k}{s(1 + T_1 s)(1 + T_2 s)} = \frac{k_p k(1 + T_B s)}{T_I s^2(1 + T_2 s)} \end{aligned}$$

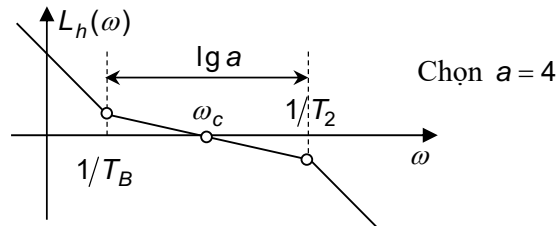
We select  $T_A = T_1$  with  $T_A + T_B = T_I$ ,  $T_A T_B = T_I T_D$ ,  $T_B = 4T_2 > T_2$ , we obtain the Bode diagram of open system as follows.

$$\omega_c = \frac{1}{\sqrt{T_B T_2}}$$

$T_B = 8, T_1 = T_2 = 2$  we imply  $\omega_c = \frac{1}{4}$ . Stability reserve of closed system  $\Delta\varphi$ :

$$\Delta\varphi = -\pi - \varphi_c = -\pi - \arctan(\omega_c T_2) - \arctan(\omega_c T_B)$$

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i. **(0.5 marks)**

The equivalent polynomial of matrix  $A$  will be:

$$\det(sI - A) = (s-1)(s^2 - 3s + 1). \text{ This system is not stable;}$$

ii. **(0.5 marks)**  $\text{Rank}(B, AB, A^2B) = 3 \Rightarrow$  This system is controllable

b) **(1 marks)**

i. **(0.5 marks)** 
$$N = \begin{pmatrix} \underline{c}^T \\ \underline{c}^T A \\ \underline{c}^T A^2 \end{pmatrix} = \begin{pmatrix} a & 0 & 1 \\ a & 1 & a+1 \\ a & a+3 & 2a+2 \end{pmatrix}$$

ii. **(0.5 marks)**  $\det(N) = -a(a^2 + a - 1)$

In order to obtain the observability property:  $\det(N) \neq 0 \Leftrightarrow a \neq 0; \frac{-1 \pm \sqrt{5}}{2}$

c) **(2 marks)**

i. **(1 marks)** State Feedback control is  $\underline{u} = \underline{w} - R\underline{x}$  với  $R = (r_1 \ r_2 \ r_3)$  satisfy

eigen values of  $(A - \underline{b}r^T)$  inside  $(-2, 0)$  and we select all of eigen values

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$$\frac{d\hat{x}}{dt} = A\hat{x} + \underline{b}u + L(y - \underline{c}^T \hat{x}).$$

ii. **(0.5 marks)** Find matrix  $L$  to obtain that  $(A - L\underline{c}^T)$  have all

eigenvalues being -3 (faster than  $e^{-2t}$ ). Using Ackermann:

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**(1d)** Drawing. The closed system is not controllable because  $\underline{\hat{x}}$  converge to  $\underline{x}$

**(0.5 d)** Selecting the state feedback controller  $\underline{u} = \underline{w} - R\underline{x}$  with  $R = \begin{bmatrix} -9 & -16 & 17 \\ 0 & 0 & 0 \end{bmatrix}$